

Control System for Less than Wind Turbines 1500W

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Abstract: Using wind power generation is another alternative for remote homes, where there is no electricity grid. Especially in Ecuador there are several places where the wind resource is really stable for the year, though at times the wind regime it becomes turbulent wind speeds become quite high exceeding 12 m / s affecting the wind turbine components.

Generally in the Ecuadorian highlands are available permanent winds of medium intensity capable of generating electricity, but by having a system of turbulence for short periods of time it jeopardizes the deployed equipment and therefore the investments made by what this study guarantees the stability of small wind turbines that are very useful in our environment to generate electricity in field type housing shelters.

Keywords: Control, Wind Generators, Protection.

INTRODUCTION

The integrity and security in the delivery of electricity from the source to the load depends largely on electrical protection system against failures and external or internal disturbances, these failures are diverse and can be overload by overcurrent or short circuit, low frequency among others.

The main function of a control system forewarn the electrical service and equipment before the failure occurs.

The components of a wind turbine are designed to last about 20 years. This means they will have to endure more than 120,000 operating hours, often under stormy weather conditions.

In our case we endeavor to design the control system, with tests corresponding operating and thus make available to society a mechanism capable enough to prevent deterioration of the components of wind generators in the middle of Ecuador and therefore the energy service is not affected due to the lack of control mechanisms on small wind turbines that are manufactured here and even lack of standards, given the experience that many of these machines being developed in our country do not care of this factor has trigger such as engine overspeed and component failure due to their high speed for short periods of time.

The energy conversion equations describing the total power generated by the wind generator designed presented. In order to validate this simulation model,

the energy conversion equations were coded with MATLAB V13.2, is used for optimization of resources to be a design tool. A block diagram approach was used during the simulation with MATLAB. In order to validate and tune output results expected at the site was used to validate the simulation program data under various conditions.

OBJECTIVES

- To avoid equipment damage due to the significant increase in lower wind speed 1500W generators that are installed in Ecuador.
- Maintain a high level of Quality of Service (stability and continuity), avoiding where possible outages.
- Design a control system capable of preventing destruction or deterioration of the internal elements of the shaft speeds of the electric generator of a wind turbine.

Mathematical Modeling

Then the block diagram of the speed control system is presented [1].

In the Figures 1 and 2, a speed control system for isolated power system is shown. The air brake controls the input speed wind turbine in order to take into account changes in load. $\Delta L(s)$ within the power distribution network. Effective rotational inertia, J , is equal to 4000 and the constant friction is very close to zero. The factor regulating the rate at steady state, R , is very small, less than 0.1. The stabilization time is 10%.

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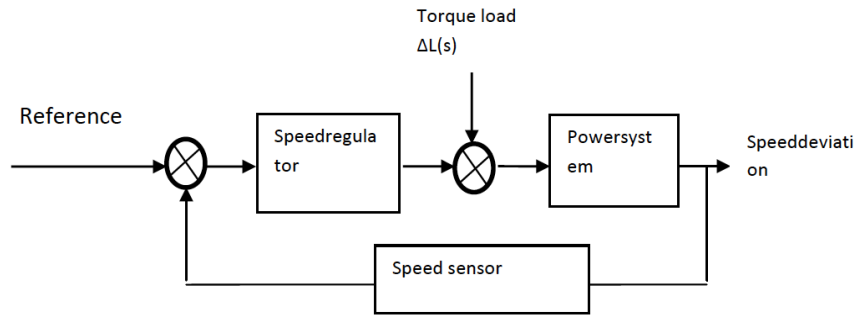


Figure 1: Block diagram of the automatic control system.

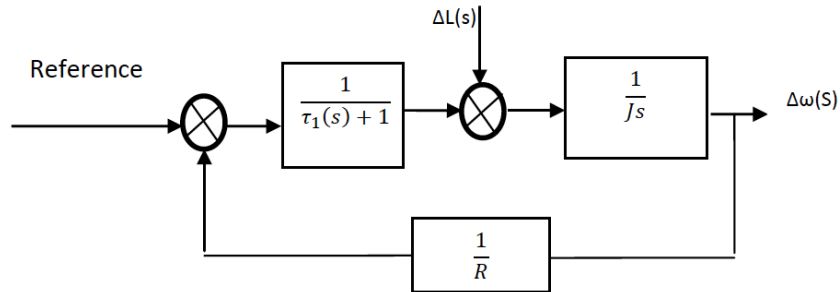


Figure 2: Block diagram in the Laplace domain [3].

We obtain the transfer function:

$$H(s) = \frac{1}{(0.1s + 1) \cdot 4000s} \cdot \frac{1}{1 + \frac{1}{(0.1s + 1) \cdot 4000s}}$$

$$H(s) = \frac{1}{400s^2 + 4000s + 1}$$

To determine whether the behavior of the system is stable, unstable or marginally stable according to the mathematical model used to simulate proceeded in Matlab identifying the locus of the roots using the command rlocus was established that the system is stable as a center especially it is far from the real axis. See Figure 3.

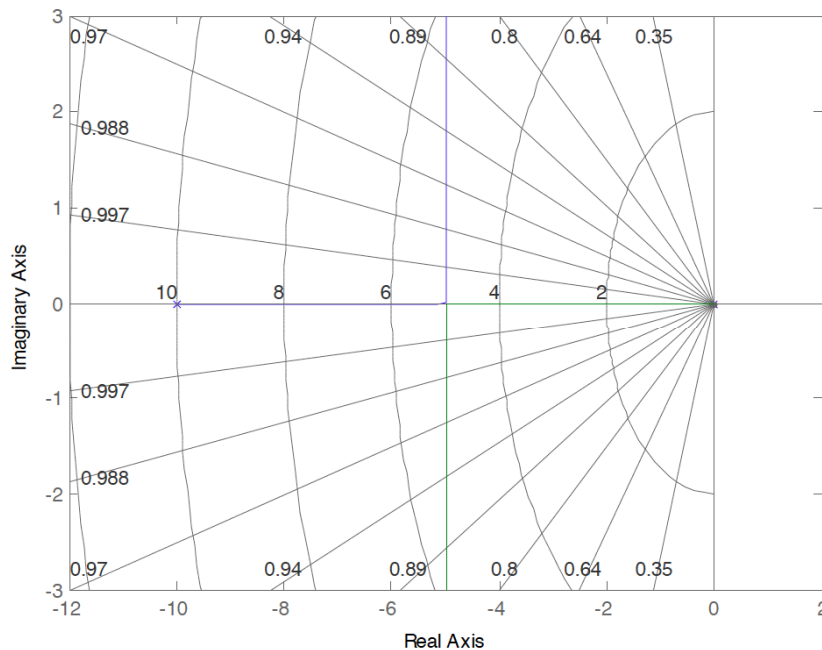


Figure 3: locus of the roots.

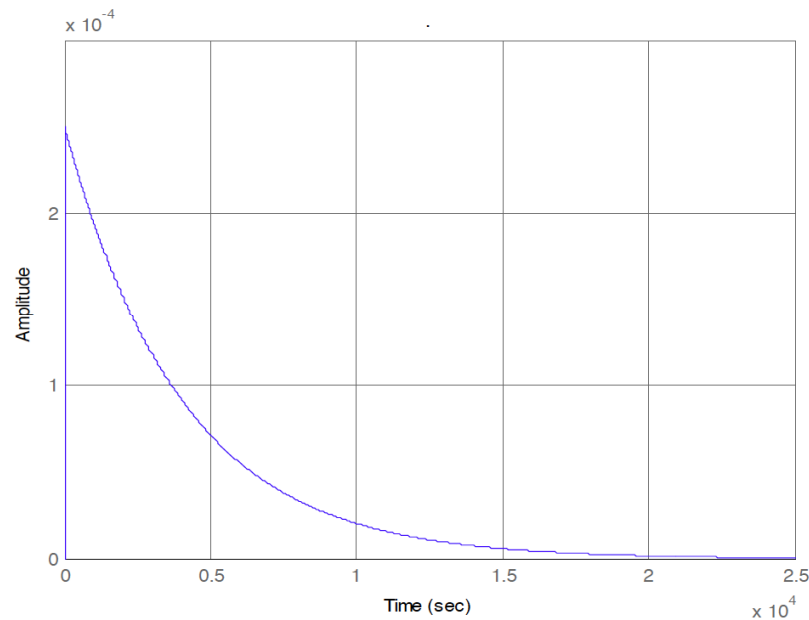


Figure 4: Impulse response.

It has also been simulated impulse response to the system and has obtained the graph No. 4 which shows the graph that gradually declines over time.

Design Phase

The control system must be different depending on the size of the turbine. For small machines, the control is simple and usually passive, on the contrary, for large machines - medium and high power - the control system will be more complicated because of the many parameters to be measured and increased accuracy required, but will represent a cost, although high, is small compared to the total system cost [2].

Thus, in our particular case passive controls make your measurements in the simplest possible way and use natural forces to act, while the active control systems using electrical and mechanical systems to achieve its purpose.

The main objectives of a control system are:

- Get automatic operation of the turbine.
- Getting the turbine to operate in line with the wind (direction, power control, etc.).
- Decide on / off the generator and successfully perform the starts and stops the turbine.
- Protect the system (overspeed, vibration, overheating, curls interconnect cables).
- To maximize system performance.

- To increase the life of the wind turbine (minimizing unintended burdens that may arise).

For the design of the wind turbine we have been divided into nine parts, the same as a specific role.

1. Aspas
2. Brake
3. Electromagnet
 - swivel
4. Base engine
5. Aspa guide
6. Tube and support base
7. lead acid battery
8. Speed sensor or anemometer
9. Electromechanical relay

The control system must necessarily include testing or diagnosis operation immediately detect a malfunction and should immediately stop the speed of the turbine, thereby ensuring system costs and service reliability.

The control system consists of three stages:

1. **Input stage:** This stage is responsible for driving signals from the speed sensor arranged on the axis of the central electrical generator to be processed immediately when too high a speed is

detected and send orders to the electromechanical actuator type shoe I acted on said axis.

detected that the speed is normal aerodynamic braking system returns to its initial state and therefore regular electricity generation.

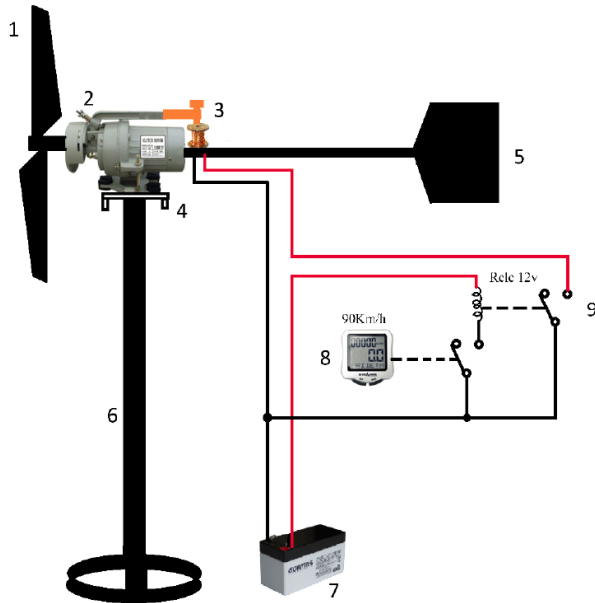


Figure 5: General diagram generation and control system.

Representative Photo of Electromechanical Control System



Figure 7: Electromechanical actuator mounted on the electric generator.

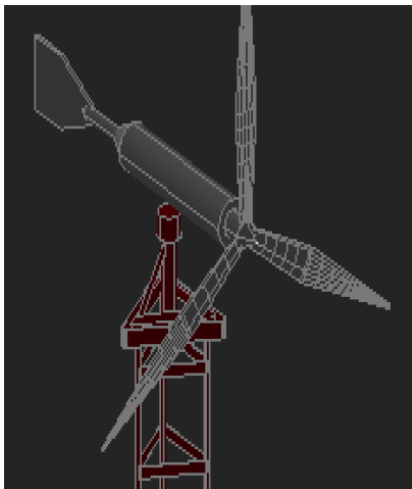


Figure 6: Wind turbine design built for testing.

2. **Warning Signs:** This stage is responsible for collecting the signals corresponding to anomalous situations in vital systems, commanding absolute priority over any other order the emergency stop of the wind, until it disappears the cause that caused the emergency.
3. **Output stage:** This stage transmits electrical signals from execution of instructions received from the control system operating the corresponding actuator (air brake). When it is



Figure 8: Overview of the wind generator control system mounted speed.

Once designed the control system and made the corresponding assembly, necessary to examine the whole system of wind power generation, describing the main formulas and simulating in MATLAB V13.2 program to verify the behavior of the theoretical curves compared measured results.

Wind Power System

The power of a particular wind turbine is given by [3];

$$P_{WT} = 0.5 * C_p * \rho_{air} * v^3 * \eta_{aer} \quad (1)$$

Where; P_{WT} = Wind power sweep produced by the blades per unit area. C_p = Betz power coefficient. ρ_{air} = Air density and v is the wind velocity.

Taking into account the internal performance of the wind turbine, the following can be written;

$$\eta_{aer} = \eta_{fmec} \cdot \eta_g \cdot \eta_{mp} \quad (2)$$

Where; η_{fmec} , η_g are mechanical friction and generator efficiencies respectively and the efficiency speed multiplication box is η_{mp} .

The power output of the wind turbine in equation (1) can be expressed in three-phase power AC as;

$$P_{3f} = \sqrt{3} \cdot \eta_{c1} \cdot U_{line} \cdot I_{line} \cdot \cos\varphi \quad (3)$$

With three phase AC power is P_{3f} , line current I_{line} , represents power factor $\cos\varphi$, and the electric conversion efficiency is referred to as η_{c1} .

Controller

Generally, the controller power output is given by;

$$P_{Cont-dc} = V_{bat} (I_{rect}) \quad (4)$$

Where; V_{bat} is multiplication of the nominal voltage DC in the battery for any particular system and I_{rect} represent the output current of the rectifier in DC.

Battery Performance Model

Normally, batteries in a hybrid system are connected in series to obtain the appropriate nominal bus voltage [9]. Therefore, the number of batteries connected in series in a battery banks is calculated as follows;

$$N_{SBat} = \frac{V_{PV}}{V_{Bat}} \quad (5)$$

Inverter, Charger, and Loads Performance Model

The characteristics of the inverter are given by the ratio of the input power to the inverter P_{inv-ip} and

inverter output power P_{inv-op} . The inverter will incur conversion losses and to account for the inverter efficiency losses, η_{inv} is used [4];

$$P_{inv-ip} \cdot \eta_{inv} = P_{inv-op} \quad (6)$$

In many applications, load may not be served with the desired amount of energy. This situation is described as loss of load probability (LLP) and can be calculated using the following equation and also, LLP can represent the system reliability [7];

$$LLP = \frac{\text{Energy}_{-}\text{Demand}}{\text{Energy}_{-}\text{Served}} \quad (7)$$

The AC power of the inverter output $P(t)$ is calculated using the inverter efficiency η_{inv} , output voltage between phases, neutral V_{fn} , for single-phase current I_o and $\cos\varphi$ as follows [8];

$$P(t) = 3\eta_{inv} V_{fn} I_o \cos\varphi \quad (8)$$

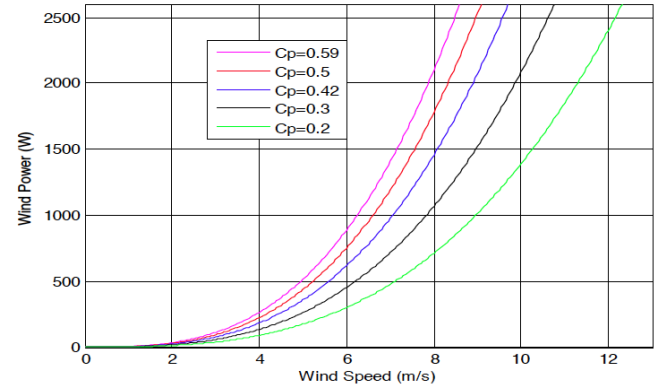


Figure 9: Power-speed curve for different values of Betz Coefficient [10].

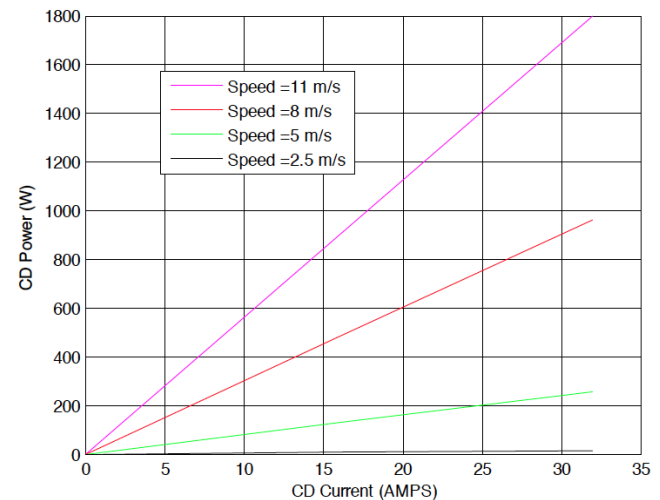


Figure 10: DC Power- DC Current for wind Speed (m/s).

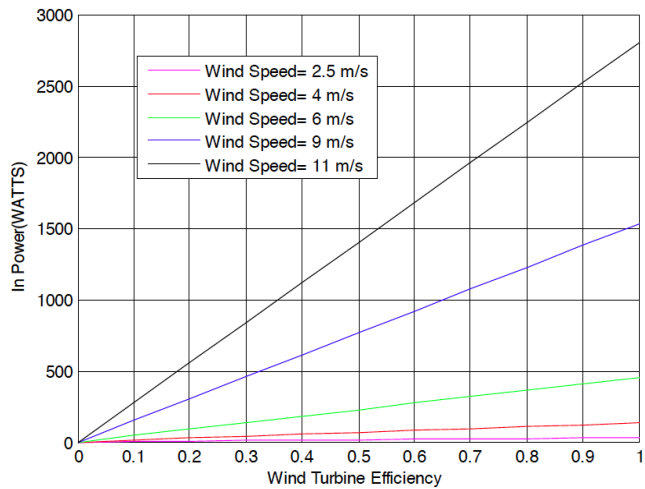


Figure 11: Energy conversion efficiency at various wind speeds [11].

Model Validation

In order to validate our numerical prediction model described, we have built a wind generator and implement mechanisms that allow for performance testing. After giving different velocities to the prototype it verified that from 14m/s the electromechanical actuator actually goes into action and thereby slowing the shaft of the electric generator, after about 4 seconds of time the speed is sensed again and down the electromechanical actuator separating from the shaft of the electric generator, so it is possible to determine that the model employed in good agreement with the director field trials.

It is quite clear from these figures that our numerical model predicted quite the drive control system.

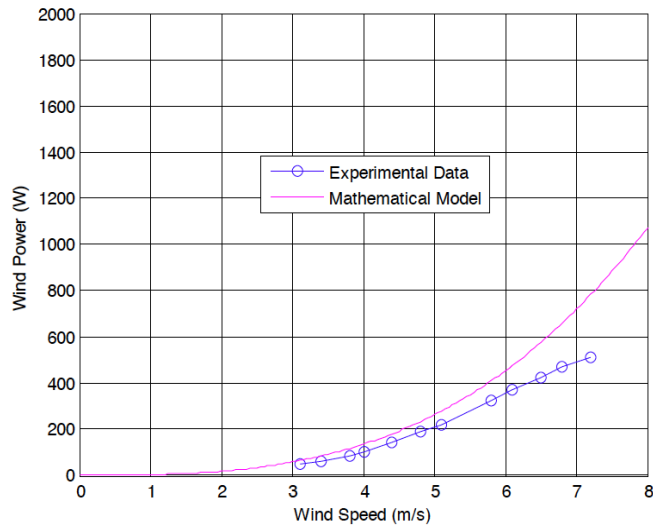


Figure 11: Comparison between Wind Turbine data (Ikhsan et al. [7]) and model's prediction.

CONCLUSIONS

For the purpose of validating the simulation model mentioned above were coded with MATLAB V13.2 and used as an optimization and design tool. A block diagram approach was used for the simulation with MATLAB. In order to validate and tune the predicted results, the in situ data were used under various conditions. The prediction model fair comparison with the data. We certainly believe that this model can be used as a tool for design and optimization with great confidence.

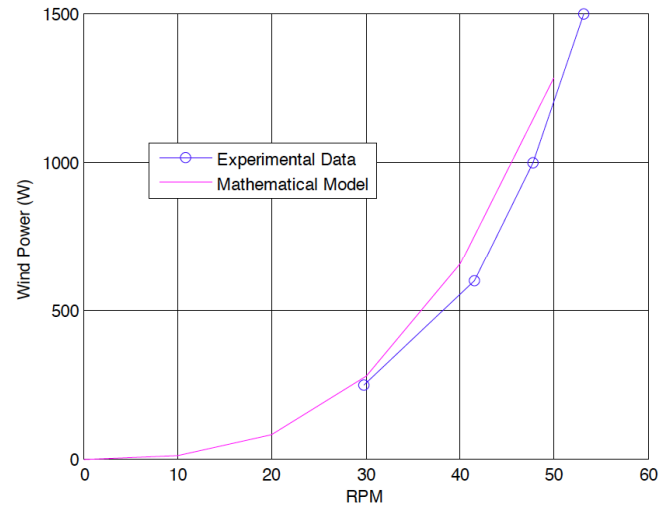


Figure 12: Comparison between Wind Turbine data (Yueqing Zonhan Wind Power Co. Ltd [5] and Bosma B. and Kallio [6]) and model prediction.

In addition, we make a comparison between the theoretical curves and concerning the most significant parameters such as wind generator power and speed experimental data.

NOMENCLATURE

- b = Coefficient of friction of the generator referred at wind turbine [N-m/rad/s]
- R = Regulation factor
- τ_1 = Time of stabilization
- $\text{Cos}\varphi$ = Power factor referred to wind turbine
- C_p = Betz power coefficient
- I_o = Single-phase current
- I_{line} = Line current referred to wind turbine
- I_{rect} = DC current to the rectifier output

J	= Inertia moment of the generator [Kg-m ²]
K	= Coefficient proportional to input kinetic energy
K_p	= Coefficient of the controller
LLP	= Loss of load probability
L_a	= Inductance of armature[H]
N_{SBat}	= Number of batteries connected in series
$P(t)$	= AC power of the inverter output
P_{3f}	= Three phase AC power of the wind turbine
P_{WT}	= Wind power sweep produced by the blades
$P_{Cont-dc}$	= Power Controller
P_{inv-ip}	= Inverter input power
P_{inv-op}	= Inverter output power
R_a	= Resistance of armature[Ω]
RPM	= Revolutions per minutes
U_{line}	= Line voltage referred to wind turbine
v	= Wind velocity
V_{bat}	= Nominal voltage DC in the battery
V_{fn}	= Phase- neutral voltage

Greek Alphabet

η_{aer}	= Wind turbine efficiency
η_{fmec}	= Mechanical friction efficiency
η_g	= Generator machine efficiency
η_{c1}	= Electric conversion efficiency is referred to wind turbine
η_{inv}	= Inverter efficiency
ρ_{air}	= Air density

Subscripts

aer	= Aero generator
Air	= Air
bat	= Battery

$Cont$	= Controller
$c1$	= Electric conversion referred to wind turbine.
fn	= Phase neutral
$fmec$	= Mechanical friction
$inv-ip$	= Inverter input
$inv-op$	= Inverter output
p	= Power
pc	= Power conditioning
rect	= Rectifier
$SBat$	= Batteries connected in series.
$total$	= Total
WT	= Wind Turbine
$3f$	= Three phase AC

ACKNOWLEDGEMENT

The research work presented in this paper was made possible through the support of the Catholic University of Cuenca.

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Received on 24-05-2016

Accepted on 10-10-2016

Published on 07-11-2016

DOI: <http://dx.doi.org/10.6000/1929-6002.2016.05.03.3>

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